

Crack Behaviour in Materials: A Comparative Study

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Abstract: Crack difficulties are important research topics for multiferroic composite media, which offer a lot of potential for producing multifunctional devices. It is put into consideration the magneto-electro-thermo-elastic coupling effect. The two crack surfaces are symmetrically loaded by a combination of homogeneous thermal, magnetic, electric, and mechanical loadings. Only the shallower region of a deep flaw in the wall structure inside the skin-depth layer impacts the initial temperature Induction Thermography (IT) response while assessing ferromagnetic constructions, but the deeper part has zero influence. This paper provides an exhaustive overview of these crack behavior studies as well as proposes a course of action for future exploration. Based on the literature, three types of crack behavior, which are magnetoelastic, ferromagnetic, and piezoelectric (PE), were explored significantly. Literature reviews have indicated that the magnetoelastic crack studied is popular among researchers around the world. Besides, the procedure and conditions are easier and faster compared to ferromagnetic and PE. Future research should therefore concentrate on the investigation effects of the magnetoelastic crack.

1. Introduction

The anti-plane fracture problem with regards to three nano-cracks emanating via a magnetoelectrically permeable triangle nano-hole in magneto-electro-elastic (MEE) materials having surface effect were rectified by building a new conformal mapping

relying on the complex potential theory as well as the Gurtin-Murdoch surface/interface model [1]–[4]. An anti-plane shear problem of an electrically and magnetically impermeable nano-elliptical hole exposed to magnetic loadings, in-plane electrical, and far-field anti-plane mechanical is detailed in

MEE materials having surface effect [5]–[7]. Li & Zhang said In engineering applications, the failure prediction of a structure depends not only on the strengths of the materials with which it is built, but also on the local stress concentrations. For brittle or quasibrittle elastic materials, it is clear that the crack initiation from a stress concentration area is a critical moment in the structure service life [8]. The cracks may have observed at some locations of high stress area due to the long operation time of turbine blades. [67]

How to quickly detect and measure the geometries of surface-breaking cracks is a recurring difficulty in critical structural maintenance. Induction thermography (IT) is a technology that could be used to detect these types of flaws [9]. The principle of the popularly utilized magnetizing-based eddy current testing (MB-ECT) sensor with regards to ferromagnetic materials is clearly stated: magnetization eradicates permeability non-uniformity and enhances penetration depth. As a consequence, non-destructive testing (NDT) is applied in a harsh manner. Thus, the surface crack's overlooked permeability distortion is highlighted and investigated at various magnetization states. An infinite plate of soft ferromagnetic, as well as paramagnetic elastic materials, is examined for a kinked crack originating from an initial crack. The distant region of the plate is placed under a

consistent magnetic field intensity. Linear magneto-elastic materials include soft ferromagnetic elastic and paramagnetic materials. The fracture failure always happens due to strong interactions among cracks or crack interconnections each other, where the strong interactions or interconnections depend on the applied external loading the geometrical configuration of cracks, such as crack sizes, crack shapes, crack locations as well as crack orientations. However, it is impossible to know the distribution information of all the cracks beforehand, particularly when the quantity of cracks up to hundreds even thousands.[68]

In aerospace, military, and other industries, functionally graded piezoelectric materials (FGPMs) are frequently employed. The study of a crack having a defined length traveling at a constant velocity along the interface of distinct piezoelectric materials (PMs) is comprehensive. The precise formulations of dynamic stress and electroelastic field, as well as electric intensity factors, are inferred utilizing the expanded Stroh formalism and Muskhelishvili's technique. PMs feature an electromechanical coupling that enables them to be employed as sensors, actuators, shape control devices (inverse piezoelectric effect), and energy harvesting devices (direct piezoelectric effect). Note that they are employed in a variety of

contemporary technological fields, for instance, the automotive and aerospace industries, and are often built in a block form or a thin laminated composite. How to quickly detect and measure the geometries of surface-breaking cracks is a recurring difficulty in crucial structural maintenance. Induction Thermographic (IT) might be a useful tool for detecting these kinds of defects. In eddy current testing (ECT), surface cracks' quantitative evaluation employing detection signals is critical for precise crack prediction. Tiny cracks are tough to assess in terms of both depth and width. For predicting the surface cracks' depth and width in ferromagnetic materials, a quantitative evaluation technique depending on Bayesian networks is presented.

This study's aim is to present a new reliable and efficient technique on the NDT field for crack characterization in non-ferromagnetic materials utilizing an electromagnetic acoustic transducer (EMAT). It is a non-contact ultrasonic technology that detects and generates ultrasonic waves in conductive materials. Service exposure, fatigue, residual stresses, corrosion fatigue, stress corrosion cracking, and other conditions can cause surface cracks in components. To identify and monitor such cracks, several NDT approaches are employed. The magnetic Barkhausen Noise (MBN) study is one method for examining microstructural anomalies or stress patterns

in situ. Stress may create spontaneous magnetic signals in ferromagnetic materials in the geomagnetic field, and the approach, called metal magnetic memory (MMM) testing, can be utilized to determine fatigue life.

The purpose of this research is to investigate how SH-waves are scattered in the piezoelectric (PE) bi-material half-space via a circular hollow between two symmetrically permeable interface cracks. Here, the steady-state response of the issue is determined utilizing Green's function approach as well as the complex function method. Moreover, the mirror method is used to generate the core statement of Green's function. This meets the criteria of becoming electric insulation and stress-free on the horizontal boundary of the orthogonal space in which the circular cavity is positioned. This includes the bearing condition of a harmonic out-plane line source force on the vertical boundary. For the design of PE components, dynamic fracture analysis of PMs with eccentric defects denotes an essential requirement. This research's goal is to propose a practical solution to the dynamic anti-plane shearing issue of PE bi-materials having permeable interfacial cracks around an eccentric circular hole. Moreover, the SH-wave's scattering issue via a circular inclusion around the two symmetrically permeable interfacial cracks in the PE bi-material half-space is studied employing the Green's function as well as complex function

methods to derive the steady-state response. With regards to combined mechanical and electrical loadings at infinity, the impacts of Maxwell stress on semipermeable periodical cracks in PMs are examined. These crack properties, which are important in modifying hydrology of soils are: width, length, depth and orientation of soil's cracks.[69]

With homogeneous remote electrical and mechanical loads, the effects of crack speed and electrostatic force on V fracture behavior are explored. An apparent hoop of mechanical (strain) energy release rate (MERR) is developed to estimate the MERR of a PE crack having an infinitesimal kink at certain given arbitrary angle, relying on the notion of the hoop field intensity factors of an initial crack preceding any kink. Numerical examples employing the boundary element method (BEM) are employed to test the efficiency and validity of the approximation that has been simplified. The traction boundary integral equations (BIEs) are employed to calculate generalized crack-opening-displacements or displacement jumps. It is critical to develop and utilize innovative NDT methods to address the initial damage testing problem of ferromagnetic materials. The MMM method, also referred to as the micromagnetic testing method, may identify faults in ferromagnetic materials like steel early on. The MMM method, however, is only appropriate for

damage localization due to a shortage of quantitative studies.

Since the magnetic fields distribution inside the ferromagnetic material is rather convoluted owing to motion-induced eddy current (MIEC) and ferromagnetic material magnetization, NDT for ferromagnetic material under motion conditions resemble a difficult problem. As a result, a rapid, accurate, as well as autonomous NDT approach for quantitative crack identification in moving ferromagnetic materials is a requirement. Presently, the pulsed eddy current (PEC) approach is frequently adopted in metals for quantitative crack characterization; yet, research on the effect of velocity on PEC is limited.

The crack-tip stress intensity factors (SIFs) in a ferromagnetic thin plate exposed to external loads are calculated utilizing an I-integral method. The magnetization distributions, integral area size, and domain walls have no effect on the value of I-integral, demonstrating its applicability to large-scale domain switching. The I-integral method is effectively utilized to achieve the crack-tip intensity factors but also decouples distinct modes of the crack-tip intensity factors in ferromagnetic thin plates having an impermeable edge crack with respect to distinct mechanical and/or magnetic loadings predicated on the magnetic and stress field acquired from phase-field simulations. Lengyel & Schiavone [10] explain that there are other

studies using in mathematics Integral equations as follows Define the complex antiplane displacement potential (ϕ) , $\equiv +$, as

$$(\phi(z)) = \frac{1}{\pi i} \int \frac{t}{t-z} \quad (1)$$

(ϕ) can be represented in the form of a Cauchy integral [11].

2. Review of study

Given their good coupling between electrical, mechanical, as well as magnetic fields, magneto-electro-elastic (MEE) composite materials provide a broad perspective of applications in current smart structures. Moreover, Van Suchtelen [1] was the first to disclose this novel phenomenon in 1972. Cracks in these materials are unavoidable due to their ceramic structure. If these cracks get larger, the material's structural integrity and/or functional characteristics may be compromised.

A molecular dynamics research of how structural flaws influence the formation and self-healing of nanosized cracks in bcc iron single crystals with respect to various mechanical stress conditions at room temperature. At the crack spots, deformation is shown to be followed by a local rise in atomic volume. The ability of structural defects to transfer excess atomic volume from crack spots to the free surface or other interfaces dictates the crack development behavior [12]. Eddy current pulsed thermography (ECPT) is a

non-destructive testing and evaluation (NDT/E) technology that is widely utilized to detect and quantify cracks in ferromagnetic pressure components. Nevertheless, in practice, stress has a major impact on permeability, despite the fact that it has not been considered. We adopt the Stroh octet formalism to estimate the electroelastic field for an anisotropic piezoelectric (PE) solid degraded by a blunt crack to increase crack detection accuracy. A parabolic cavity having a charge-free and traction-free boundary represents the blunt crack itself. Because of their unique electromechanical coupling properties, piezoelectric materials (PMs) have a wide range of uses, but their brittle nature makes them prone to unexpected failure. The fracture of PMs under various application conditions has piqued the curiosity of scholars. Propeller blades, transducers, sensors, energy harvesters, vibrators, and electromechanical actuators are all examples of applications where PMs are employed. These materials are handled in numerous forms of cyclic loading, while crack growth analysis is very valuable in predicting material life. Given their electromechanical coupling response, PMs are widely utilized in modern science and technology. PE devices with defects can experience fracture or failure during servicing operations due to the stiff and brittle nature of some PMs. Subsequently, it is considered essential to examine the failure behaviors induced by defects like cracks and holes.

Considering PMs are mostly utilized as sensitive components, defects, for instance, cavities, cracks, and inclusions possess a significant impact on the materials' applicability. Sensors, actuators, nano- and micro-electromechanical systems, as well as other PE components are often made from blocks or thin laminated composites. During material processing processes, many voids and cracks were formed, interacting with one another and impact the service performance of PE components. With regards to combined mechanical and electrical loadings at infinity, the Maxwell stress influence on semi-permeable periodical cracks in PE material is investigated. For a plane-strain problem of a crack between two distinct PMs exposed to an electrical displacement and tensile mechanical stress presented at infinity, an arbitrary polling direction of the top material is taken into account. Electrical conditions at the crack faces with constrained permeability are factored in. Engineering structures frequently employ ferromagnetic materials. Damages incurred during the manufacturing process and the usage of ferromagnetic materials might jeopardize the engineering structure's safety and potentially result in catastrophic industrial mishaps.

The relative motion between the detection devices and the ferromagnetic material caused the motion-induced eddy current (MIEC) to be formed. The drag effect

would appear, resulting in a rather complicated magnetic field distribution in the ferromagnetic material compared to quasi-static or static testing. As a result, a multi-crack electromagnetic nondestructive testing (NDT) probe for high-speed moving ferromagnetic materials is immediately needed. Engineering structures frequently employ ferromagnetic materials. Damages incurred during the manufacturing process and the usage of ferromagnetic materials might jeopardize the engineering structure's safety and potentially result in catastrophic industrial mishaps. It is critical to design and implements innovative NDT methods to address the initial damage testing problem of ferromagnetic materials. The metal magnetic memory

(MMM) method, also referred to as the micromagnetic testing method, is capable of detecting damage in ferromagnetic materials like steel early. The MMM method, though, is only appropriate for damage localization given the lack of quantitative study.

A conductive tunnel crack and a remote strip electrode located at two PE semi-infinite spaces interfaces are investigated. An in-plane electrical field parallel to the interface and an anti-plane mechanical loading is applied to the bi-material. The research of the dynamic antiplane properties of a radial crack originating from a circular cavity in PE bi-

materials, With regards to the influence of anti-plane mechanical loading and an in-plane electrical field parallel to the crack faces, an electrically conductive crack between two semi-infinite PE spaces is examined. This issue has a precise analytical solution, where the oscillatory singularity at the crack tips is exposed. The Gurtin–Murdoch surface/interface model is employed to analyze an electrically permeable elliptical nano-hole or nano-crack implanted in an infinite PE material having surface effect, which is exposed to in-plane electrical loads and far-field antiplane mechanical. Applying complex function theory, the problem is simplified to a linear relationship problem. A unique inclined excitation approach for eddy current thermography was presented to remove the “fuzzy effect” in combination with wavelet singularity-based image segmentation, which has a negative impact on crack detection, particularly for nonferromagnetic materials. At various crack depths and widths as well as heating periods, the efficacy of crack detection having parallel and inclined excitation was quantitatively evaluated.

2.1. Magnetoelastic

In ferromagnetic materials, magnetic and mechanical properties are strongly coupled. The application of stress causes magnetization to be sensitive, resulting in considerable implications on the operation of electromagnetic devices [13]. Magnetoelastic sensors (MES) have received

a lot of interest; since they are wireless and passive, they may be employed in a variety of biomedical sectors [14].

Under the magnetoelectrically impermeable and permeable boundary conditions, the exact solutions of the stress intensity factor, the magnetic induction intensity factor, the electric displacement intensity factor, as well as the energy release rate are achieved. Under two distinct boundary conditions, the numerical examples indicate the impact of the surface effect on the stress intensity factor, the magnetic induction intensity factor, the electric displacement intensity factor, as well as the energy release rate. Note that the surface effect causes electric, stress, as well as magnetic field coupling. Here, as the cavity size increases, the importance of the surface effect decreases until it approaches the classical elasticity theory [12]. The results are in line with previous research by K. Jangid, who suggested a numerical problem that is then solved utilizing the Riemann–Hilbert method to yield the electric displacement, stress, as well as magnetic induction components at each location in the domain. Furthermore, the crack opening potential drop, the crack opening displacement, crack opening induction drop, as well as intensity factors are all given specific expressions. For the (Formula presented) composite, a numerical contextual analysis is provided. The numerical analysis shows that changing the magnetic/electric poling

directions has an impact on the crack parameters [13]. This study offers a DC-biased magnetization-based induction thermography (DCMIT) approach for ferromagnetic materials that extends the visible depth range of standard Induction Thermographic (IT). Depending on permeability distortion in the skin-depth layer, DCMIT may be able to create a monotonic connection between the defect depth and the thermal feature. Here, when the coil direction is parallel to the length direction of the notch, DCMIT can then quantify the notch with a maximum depth of 6.0 mm, but standard IT may just barely accomplish this depth detection [14]. The goal of this study was to test and validate a fundamental perspective on the interaction of multiple cracks on magnetoelastic material fracture behavior. A soft ferromagnetic material degraded by an array of periodic cracks is explored theoretically under in-plane magnetic loading. Here, the conformal mapping method and the analytic function boundary value theory are employed to construct a rigorous analytical solution for the stress and magnetic fields. The closed-form equations for the field intensity components are provided. Utilizing numerical examples of magnetically permeable and impermeable cracks, the link between the mode-I stress intensity factor, the cracks' period ratio, the surrounding medium, as well as the applied magnetic loading is studied. The analytical solution

obtained in this work may be utilized as a theoretical benchmark for the fracture of a magnetoelastic solid with many defects [7].

Detailed expressions for the field components at a general point in the deformation of magneto-electro-elastic media by a stack of parallel, anti-plane shear cracks to which nonuniform mechanical, electric, and magnetic loads are implemented and deduced in closed-form utilizing a generalized technique of continuous dislocation distributions. As an outcome of their angular variations around a crack tip, comprehensive, new representations for the suitable electric displacement, stress, as well as magnetic induction intensity components are developed. There are graphical representations of representative numerical findings. The crack shielding effect is illustrated in this video. Validation of this analysis is regarded to be limiting exceptional instances [9]. This is backed by research by Stoyanov Y., which reveals that the solution method is the boundary integral equation method (BIEM), which is initially evaluated against benchmark cases before being utilized in numerical simulations. The numerical solution is constructed utilizing Mathematica program code. Numerical simulations show that the dynamic stress concentration field is dependent on the linked nature of the active composite material, incident wave parameters, nano-

crack size, and surface and bulk material characteristics [15]. The crack's electric and magnetic permeabilities are idealized to be totally permeable (or impermeable), and four boundary conditions are explored as a result. With the generalized approach of potential theory, the field variables in 3D space, as well as several parameters of major importance in fracture mechanics, are determined analytically. For each of the four scenarios, a unified solution of the field variables is proposed. The finite element formulation is also described using the virtual displacement approach. The present analytical solutions are validated using numerical findings generated from analytical methods and simulations, and the effect of magneto-electro-thermo-elastic characteristics is discussed [16]. The discovery is in line with Liu Y's previous research findings. The complex function technique and conformal mapping methods are employed to provide precise closed-form solutions of the electric displacement, stress, as well as magnetic induction intensity factors close to the crack tip when the nano-elliptical hole is transformed to a nano-crack. For PE, PMs, and MEE materials with surface effect, numerical examples are given to indicate the impacts of nano-crack size on the field intensity factors close to the fracture tip produced by magnetic, electrical, and mechanical loadings. The interplay of the electric, stress as well as magnetic fields

around the nano-hole is studied. The findings indicate that when the nano-crack size increases, the resulting solution approaches the classical elasticity solution [17].

In general, functionally graded MEE materials are subjected to an anti-plane timeharmonic load. Here, the goal is to investigate how the imposed external load's frequency influences the stress concentration around the fracture points. A boundary value problem for a partial differential equations system is used to define the mathematical model. To achieve fundamental solutions in closed form, a Radon transform is used. As per Wang and Zhang, the boundary value problem for the PE condition may be reduced to a set of integrodifferential equations along the crack. Employing instances from the literature, software code in FORTRAN 77 is written and validated for the numerical solution. In simulations, the stress intensity factors (SIF) for various types of crack dispositions, load, as well as the direction and magnitude of the material gradient are demonstrated to be dependent on the frequency of the incident wave [18].

Magnetically-responsive iron-based particles of varying chemical compositions and sizes are used as additives to heat up road pavements causes close fractures to have different effects as per Jeoffroy E. Utilizing an alternating magnetic field

(AMF), we observed that based on the particle electrical conductivity, The temperature on the surface of asphalt samples reaches its maximum at a certain size. Even though the particles are equally dispersed after mixing, when subjected to the AMF, asphalt samples containing bigger particles show inhomogeneous heating. The ability of asphalt materials containing iron-based particles to heal was established by mechanical recovery of samples during a twofold torsion test after and before exposure to the AMF. We propose design parameters for magnetically responsive asphalts for enhanced-durability road pavements based on these findings [19].

The multi-source effect of the magnetizing-based eddy current testing (MB-ECT) method is investigated in this research utilizing the equivalent source methodology. The primary magnetic leakage field, permeability distortion surrounding the crack as well as the secondary disturbed magnetic field created by the fracture form the disturbing magnetic field source. Using finite element analysis (FEA), the influence of the magnetizing current and probe lift-off is also studied. As a result of the permeability distortion, the simulation result reveals a “concave” feature. The prominent signal components are analyzed in a series of experiments under various settings. The magnetizing current selection corresponds to a

unique form when charting the signal amplitude as a function of the magnetizing current and probe lift-off in the MB-ECT method. (Ran et. al, 2019) discovers the multi-source effect in the mechanism of MBECT sensors, as well as the key theory or analytical principles for precise crack evaluation

[20]. However, Liu H. eventually proved that this work yields the non-local theoretical solution to a 3D rectangular permeable crack in magneto-electro-elastic materials (MEEMs) utilizing the Schmidt approach and the generalized Almansi’s theorem. The issues are presented as three sets of dual integral equations utilizing the Fourier transform. Moreover, the elastic displacement, electric potential, and potential magnetic jumps along the fracture surfaces are unknown factors. The displacement leaps over the crack surfaces are instantly extended as a sequence of Jacobi polynomials. Moreover, the resultant equations are solved utilizing the Schmidt approach in solving the dual integral equations. Numerical examples of the impacts of the rectangular geometric shape cracks and the lattice parameter on electric displacement, stress, as well as magnetic flux fields at the fracture edges are presented in MEEMs. In contrast to the conventional solution, recent MEEMs solutions possess no electric displacement, stress as well as magnetic flux singularities at the crack margins [21].

The wavelet energy's relative entropy of MMM signals is based on the functions of time-frequency localization of information entropy and wavelet transform reflecting the source information uncertainties. It is suggested to expressed fatigue crack propagation based on the attributes in crack propagation of ferromagnetic materials. In the experiment, the wavelet energy's relative entropy is examined. Wavelet energy relative entropy is a sensitive indicator of crack progression, according to the results. The changing area of relative entropy of wavelet energy may be utilized to calculate the crack propagation length. As per fracture analysis [22], the crack depth is proportional to the relative entropy of wavelet energy. Consequently, Hasebe N. has also shown that having to analyze this magneto-elastic stress problem, stress field, paramagnetic field intensity and the ferromagnetic field intensity generated from Faraday's equation of magnetic force line (uniform and pure shear stress state) are employed, accordingly. The effect of all three procedures is equivalent: a uniform, pure shear stress condition. Soon after the fracture begins, the kinked crack angles are attained in either direction of magnetic field intensity. The $0 \leq \delta \leq 360^\circ$ directions are put into consideration.

- (i) The kinked crack stimulates in the direction that takes the maximum value of the Mode

I stress intensity factor shortly after the crack initiation, provided that the Mode I stress intensity factor is positive;

- (ii) the kinked crack initiates in the direction that meets the Mode II stress intensity factor;
- (iii) the kinked crack initiates in the direction that meets the Mode III stress intensity factor.

The starting angles are determined to be between $-150^\circ \leq \theta \leq 150^\circ$. It is stated that these factors yield a similar outcome for kinked crack angles. Furthermore, the distributions of stress and magnetic field intensity are examined for certain kinked fracture angles as well as magnetic field intensity directions. The stress intensity variables for magnetic field intensity specific directions are also analyzed vs. the fracture length for particular kinked crack angles [23]. Only the thermo-magneto-electro-elastic basic field in infinite space, which comprises a pennyshaped crack exposed to a pair of point temperature loads across the lower and upper crack lips, has been assessed utilizing this approach. The material is transversely isotropic, and the break is assumed to be in the isotropic plane. For the crack with magnetically and electrically impermeable qualities, the integral boundary

equations are carefully solved. The ensuing thermo-magneto-elastic fundamental fields are obtained in aspects of elementary functions. The generalized stress intensity factors, generalized normal stresses, crack surface displacement, as well as other critical fracture mechanics characteristics, are all clearly described [24].

2.2. Piezoelectric (PE)

The crack-division and conjunction method technology are then utilized to generate the first type of Fredholm integral equation having unknown anti-plane forces, which is predicated on splitting the bi-material medium into two parts along the vertical boundary. The answer is then discovered by truncating the integral equation and solving an algebraic problem with finite terms. Lastly, numerically estimate the dynamic stress intensity factor (DSIF) at the crack tip and the dynamic stress concentration factor around the circular cavity's boundary. This is employed to investigate the impact of circular cavity position, crack location, crack length, and incident wave frequency on the dynamic stress concentration factor and DSIF [25]. The results are consistent with previous research by Kumar R, and the goal of this work is to use the extended finite element technique (XFEM) to analyze an angular and straight crack repair in a structure utilizing a PE material under thermo-mechanical loading. This gives a simplified and straightforward technique for modeling a crack in a structure in order to

assess repair options. In regards to design/methodology/approach, to represent fracture geometry, the extended finite element approach is applied. The crack surface is modeled utilizing the Heaviside enrichment function, whereas the crack front is modeled utilizing branch enrichment functions. Also, the J-integral and the SIF are employed to evaluate the repair's effectiveness. The critical voltage where the patch repair is most successful is determined and displayed. The best patch design, patch placement, adhesive thickness, as well as adhesive modulus are calculated for effective repair in a thermo-mechanical stress environment. The originality or value of the numerical simulation and modeling capabilities of the XFEM technique is particularly relevant for investigating crack repair in 2D and 3D structures employing PE patch material under thermomechanical pressure [26].

Utilizing principles discovered in the Stroh octet formalism, we get full-field and explicit formulations for electric displacements and stresses having potentially applicable everywhere in the material. Moreover, we acquire real form representations of electric displacements, electric fields, strains, stresses, as well as rigid-body rotation, particularly near the point of the blunt fracture (for example, at the vertex of the solid parabolic boundary) [27]. As per his discoveries, An N's study aims to develop a reliable methodology for

determining the stress concentration at the tip of permeable interfacial cracks close to the circular hole in functionally graded piezoelectric materials (FGPM) bi-materials. The structure is loaded by an anti-plane incident SH-wave, while all material attributes are expected to conform exponential fluctuations. Fracture analysis is accomplished utilizing the Green function approach, which is utilized to address the boundary conditions problem. Apart from that, the crack mechanical model is developed utilizing crack-deviation and crack-conjunction processes, which reduce the crack problem to a set of Fredholm's integral equations of the first kind. The DSIFs at the outer and inner crack tips may be calculated. By comparing the current approach to references, the legitimacy of the method is confirmed. The geometry of cracks and circular holes, incident wave characteristics, and material inhomogeneity are all parametrically reliant on DSIF's nonnumerical situations. The technique recommended in this research overpowers the limitations of utilizing dual integral equations in dealing with asymmetric defects, paving the way for future fracture study in FGPM with more complicated defects [28].

The stress concentration at a permeable interfacial crack tip near an eccentric elliptical hole in PE bi-materials during anti-plane shearing is investigated. Fracture analysis is carried out utilizing conformal mapping and Green's function methods, both of which are

employed in solving the boundary conditions problem. Furthermore, the crack-deviation and interfaceconjunction methods are employed to construct the mechanical model of the interfacial crack reducing the crack problem to a series of Fredholm's integral equations of the first kind. Here, the DSIFs at the outer and inner crack-tips may be calculated. The technique's authenticity is validated by contrasting it to a crack that appears from the edge of a circular hole. In numerical examples, the shape of eccentric elliptical holes and interfacial cracks, incident wave characteristics, equivalent PE elastic modulus, as well as PE parameters are all parametrically reliant on DSIFs. The findings reveal that the eccentric distance exerts a considerable influence on the stress concentration at the crack tip. This might be detrimental to PE materials and devices in regular use. Moreover, the strategy recommended in this work has a broader range of applications and may be utilized to handle non-eccentric issues [29]. As per Liu H., a nonlocal stress and electric displacement solution exists in a 3D semi-permeable rectangular fracture in infinite orthotropic piezoelectric materials (OPMs). The boundary problem is created using three sets of dual integral equations. The 2D Fourier transform and modified Almansi's theorem are used to calculate the displacement jumps across the fracture surfaces. The Schmidt technique is employed in solving the dual integral equations. Hence, the non-local stress field (NSF) and non-local electric

displacement field (NEDF) are estimated along the fracture edges. The impact of the rectangular crack size, the lattice parameter, as well as the electric permittivity of the air inside the crack on the NSF and NEDF at the crack edges in OPMs is well discussed utilizing numerical data. In the existing non-local solutions. There are zero stress or electric displacement singularities at the fracture edges, which might be valuable in future research [30].

The finite element method (FEM) is implemented to analyze 3D planar cracks and nonplanar defects in PMs. A variety of plausible 3D fault models are built based on practical engineering. In contrast to the standard 2D plane as a 3D defect form, the current study considers the many causes, concrete positions, and diverse shapes of often encountered 3D non-planar defects in practical engineering. The influences of 3D defect geometry and distinct electromechanical coupling boundary conditions on the distribution of stress, electric field strength, and electric displacement around the defect are examined by shifting the geometric size of the defect and the electromechanical boundary conditions. The findings of the calculations demonstrate that the geometry of the defect and the boundary conditions have a substantial impact on the electromechanical characteristics. Additionally, the distribution

of electromechanical properties in the in-depth position of several 3D defect models is investigated, allowing for a precise assessment of the defect's fracture-prone site. This research may be utilized as a reference for 3D defects and the service life of PMs in real-world engineering structures, according to the authors [31]. Pamnani G used XFEM to investigate trilayer plates in PMs with interface cracks and came up with similar findings. Under mechanical and electromechanical stress conditions, impermeable static cracks at the interfaces of PZT-5H and PZT-4 were examined. The (oscillating) singularity fades, and a class singularity forms for the present material combination, according to numerical calculations. To acquire the stress and electric fields near the crack tip, enrichment functions for the class are used. The fracture parameters are also analysed using an integral interaction approach. The impact of mechanical and electric loading on stress and electric displacement intensity parameters has been investigated [32].

The finite element approach was employed to study the static 3D cracks in the PE material. To model cracks, crack front elements enhanced having the new six folded enrichment functions are employed. Laurent-like series were utilized to produce these functions from a semi-infinite crack analytical solution in a PE domain. A domain-based

interaction integral is utilized to derive the mixed-mode stress intensity parameters. The auxiliary electrical, as well as mechanical fields in the interaction integral, are also derived utilizing the Stroh formulation. The XFEM software is a MATLAB program that analyzes SIF and EDIF in 3D domains. The XFEM formulation is demonstrated utilizing static planar pennyshaped cracks and common solutions from the literature for Mode I SIF as well as Mode IV EDIF. Thus, the error in Modes IV and I is 0.1444 and 0.0476, accordingly. The XFEM prediction results are pretty close to the analytical projections. Furthermore, simulations of diverse cracks, for instance, inclined penny-shaped cracks, lens-shaped cracks, and elliptical cracks, have been performed in the hopes that the present technique may be useful to mechanical designers and engineers [33]. In addition, Kumar R examined the utilization of PE material to mend a crack in a structure under a thermo-mechanical stress environment and reached the same result. Cyclic mechanical stress is imposed on a plate having a straight and angular crack in a fixed temperature setting. Two scenarios were explored for the repair of cracks under (a) mechanical loading and (b) thermo-mechanical loading conditions. A V sensor is employed to calculate the voltage. Apart from that, the measured voltage is utilized to determine the SIF in both passive and active modes.

The impact of a single and double PE patch is investigated in an attempt to fix the plate. The double PE patch has been shown to be highly efficient than the single patch when placed symmetrically offset from the crack. Then, an optimal voltage and phase difference is calculated for the most satisfactory crack mending. Upon altering the placement of the PE patch in regard to the fracture site, the best-suited placement for effective crack repair is provided. Under thermo-mechanical loading, the feasibility of PE repair is investigated. The active mode of PE repair has been shown to be efficient under thermo-mechanical loading [34].

By employing sectionally-analytic functions to present electromechanical quantities at the interface, the issue is simplified to a combined Dirichlet-Riemann boundary value problem. Except for some 1D integral calculations, the solution to this issue is discovered in an analytical form. The crack faces displacement jump, the stress, the electric field, and their intensity components are all represented in closed form. These presentations are utilized to compute the energy release rate. The obtained solution is contrasted to a simple, specific case of a single crack with no electrode, exhibiting excellent agreement. An auxiliary plane issue for closed as well as open fissures between two isotropic materials is also examined. Since the mathematical model for this issue is similar to the preceding one, the deduced solution is

adopted. There is a lot of agreement when it is contrasted to a finite element solution to a comparable situation

[35]. In comparison, Liu H. employed Almansi's theorem to derive the dynamic intensity factors for multiple permeability Mode-I fractures in the PMs' plane. The present issue is divided into two sets of dual integral equations utilizing the Fourier transform. Dual integral issues are solved utilizing the Schmidt approach. DSIFs and dynamic electric displacement intensity factors (DEDIFs) are given at the crack tips. Also, on DSIFs and DEDIFs, the impacts of crack length, the distance between two parallel cracks, as well, and the circular frequency of incident waves at crack tips are exhibited [36].

Green's function and coordinate transformation methods are employed to solve Fredholm's equations in this article. The DSIFs at the inner and outer tips of the left crack is represented analytically utilizing conjunction and crack-deviation procedures. The dimensionless wave number of the incident wave, the ratio of the crack length to the hole radius, the PE parameters, and the impacts of the eccentric distance are all graphically displayed as examples [37]. Moreover, Craciun E. also evidenced how to describe and solve the mathematical problem of anti-plane cracks in

a pre-stressed and pre-polarized PE material with initial static fields, assuming that the deformed configuration of the body is locally stable. The boundary conditions of anti-plane cracks are utilized to derive the Riemann-Hilbert problems. With an unknown complex potential, nonhomogeneous linear complex differential equations can be obtained. For constant levels of imposed incremental forces, stress fields, incremental displacement, and complex potentials corresponding to the third mode of the classical fracture may be determined.

The interaction of two collinear, unequal cracks in a pre-polarized and pre-stressed PE material is also explored [38]. This paper discusses the anti-plane fracture problem of an FGPM strip with randomly distributed properties. The FGPM's elastic stiffness, PE constant, and dielectric constant are expected to vary consistently along with the thickness of the medium, and the strip is exposed to anti-plane mechanical and in-plane electric impact loadings. The FGPM, anti-plane crack problem, is simplified to a set of singular integral equations that may be solved numerically utilizing the Fourier transform and unknown discontinuous functions specified across the fracture surfaces. The impacts of nonhomogeneous and geometric characteristics on the electric displacement intensity factors and stress, as well as the impacts of nonhomogeneous and geometric features on the electric displacement intensity factors and

stress, are addressed [38]. The above findings are diametrically opposed to An N.'s findings. Crack-deviation techniques, interface conjunction techniques, conformal mapping method, and Green's function method were employed to yield a set of first-order Fredholm's equations, which are utilized to theoretically describe the DSIF at the outer and inner fracture points in V bi-materials having two interfacial fractures near an eccentric elliptical hole. Visual demonstrations of the impacts of the PE parameter, efficient PE elastic modulus, dimensionless incoming geometric parameters and wave number on the DSIF at both tips were made. Prior study is limited, particularly when the center of the hole deviates from the interface. As an outcome, the influence of eccentric distance on DSIF is examined in this study. The solution to this issue grants a more precise as well as effective method of exploring the dynamic fracture characteristics of PMs, and it has substantial theoretical implications in engineering design [39].

Relying on the investigation of the dynamic anti-plane characteristics for radial cracks originating from a circular cavity in PE bi-materials, this study aimed to develop a mechanical model of interfacial cracks originating from an eccentric circular cavity. The green function approach, coordinate transformation method, crack-deviation and conjunction approaches are utilized to solve Fredholm's equations and quantitatively define

the DSIF. The numerical solutions of DSIFs are shown and described employing numerous physical and geometric parameters utilizing a Fortran program. Moreover, eccentric flaws in materials are more prevalent and more complex to correct than non-eccentric defects. As per numerical tests, the eccentric model's DSIF at the fracture tip is larger than the non-eccentric model's, implying that the eccentricity of the cavity is more prone to encourage damage and crack growth to PMs. As a consequence, both theoretically and practically, investigating the fracture behavior of materials with eccentric flaws is critical [40]. This, nonetheless, coincides with a study by Pei P., who employed an analytical technique to investigate different PMs with periodic cracks in the presence of homogeneous electromechanical loads while accounting for the Maxwell stress. Conformal mapping and Stroh's formalism are employed to generate electric and stress fields for semi-permeable fractures with a constant dielectric value. An approximation strategy is constructed to produce the analytical solution to the crack opening displacement, which is confirmed by the pre-existing solution and numerical integral. Also, the technique described in this research yielded findings for the electric displacement field in cracks, stress, and electric displacement intensity factors. Apart from that, the numerical results portray a uniform electric displacement field inside cracks that is independent of fracture size or distribution once static uniform

electromechanical loads are imposed. Additionally, the field intensity of a periodic crack is demonstrated to be equivalent to that of a single interfacial crack when the crack spacing is greater than four times the crack length [41].

Scholars may evaluate the integrity of these innovative materials under more realistic crack surface multifield operating situations utilizing a friction-based fracture surface contact formulation. The dual boundary element method (BEM) is employed to simulate frictional fracture surface contact on PE substances in the presence of electric fields, considering the electrical semi-permeable boundary conditions on the crack. Furthermore, the formulation incorporates contact operators over the augmented Lagrangian to enforce contact restrictions on the fracture surfaces. Also, the BEM appears as an appropriate method for these interface interaction problems since it only perceives the boundary degrees of freedom. This allows for a reduction in the number of unknowns and precise outcomes having a much lower number of elements than formulations premised on the standard FEM or the eXtended finite element method. Besides that, the capability of the technique is demonstrated by solving many benchmark problems [42]. The findings are consistent with a prior study by Zhu S, who discovered

that around many FGPMs' cracks exposed to the mechanical field, electric field strength and electric displacement were enhanced. Depending on constitutive relations, geometric relations, and FGPMs' boundary conditions, the material parameters of FGPMs are measured employing a layering technique having continuous characteristics along the gradient direction in the model. Note that the numerical calculations indicate that crack distribution, crack distance, crack size, and crack angle are all essential factors in the FGPMs plate. Moreover, by evaluating the fracture properties around the cracks in the mechanical field, they may be utilized as a baseline for the FGPMs service life [43].

In terms of design/methodology/approach, the problem is split into two sets of dual integral equations utilizing the Fourier transformation. The fracture surface displacement jumps are the unknown variables. The non-local electric displacement fields and dynamic nonlocal stress are generated around the fracture tips, according to the findings. On the full dynamic fields around the fracture tips, the impacts of the distance between the circular incident waves frequency, the lattice parameter, and the two collinear cracks are numerically demonstrated. The existing solution in PMs displays zero stress and electric displacement singularities at the

fracture spots, unlike conventional solutions. Maximum electric displacement and maximum stress have been discovered to be useful as fracture criteria [44]. The findings of Onopriienko O's research also point to a novel non-oscillating model for a conductive interface fracture is also being developed. Moreover, the development of a mechanically bonded zone at the conducting crack tip exhibiting zero crack face displacement jump is the basis for this concept. The length of this zone is determined by the status of a

smooth crack closing. An explanation of the conductive crack formation mechanism confirms the validity of the bond zone model. There are some ideas for applying the suggested model to analyze infinite and finite-sized bodies with electrically conducting interface cracks [45].

The dynamic non-local theoretical solution to a limited-permeable mode-I fracture in PMs involves exposing the crack surfaces to harmonic stress waves. The Schmidt approach and the extended Almansi's theorem are employed to achieve this. Utilizing the Fourier transform method, this issue is reduced into linked dual integral equations. Moreover, the dynamic non-local stress, as well as dynamic non-local electric displacement fields at the crack points, are gained by solving the resultant dual integral

equations. Utilizing numerical findings, the impacts of crack length, lattice parameter, harmonic wave characteristics, as well as the electric permittivity of the air inside the crack on the dynamic NSF and NEDF near the crack tips in PMs are documented and addressed. The proposed electrically permeable fracture mode is more applicable than the known electrically permeable crack mode [46]. This is supported by Mishra R's study, which illustrates how PE components react in a thermo-electromechanical stress environment with many cracks. The XFEM was utilized to explain geometrical discontinuities having crack interaction. Apart from that, in this work, thermoelectromechanical challenges were divided into thermal and electro-elastic difficulties. The temperature distribution was gained by solving the heat conduction equation, which was then utilized as an input to the electro-elastic problem. In the post-processing phase, the stress intensity factors were estimated utilizing the integral interaction method as well as the simplified Stroh formalism. The methodology was implemented using MATLAB code created in-house. Using the proposed method, a set of scenarios for crack interaction research were provided [47].

The fracture of a rectangular plate of functionally graded piezoelectric/piezomagnetic material is researched. Here, the physical characteristics

of FGM are thought to evolve with time on the axis-x. Furthermore, the impermeable and permeable varieties of magneto-electric crack surfaces are considered. The issue is reduced to power-series equations using a semiinverse method. The boundary collocation method is utilized as a numerical approach to compute these equations in the finite region. Utilizing magneto-electric loads and two types of crack surfaces, the impacts of the gradient parameter on fracture behavior are investigated. A rise in the gradient parameter is linked to a reduction in FGM's capacity to fracture. Enhancing the magnetic load instead of the electric load helps crack initiation and development. With respect to the magneto-electrically permeable assumption, electric and magnetic loads possess no influence on the potential field in regards to the crack singularity. When the impermeable type is present, however, magnetic and electric loads serve a major role in the crack tip singularity [48]. Other than that, Pamnani G's prior work, which employed an extended FEM to examine a static impermeable fracture at the interface of PMs, produced comparable outcomes. An edge crack and a center crack at the interface of PZT-5H and PZT-4 for the kclass singularity of PMs were explored under mechanical and electromechanical loadings. Kclass enrichment functions are employed to identify the asymptotic fields around the crack tip. Furthermore, KI and KIV are

calculated utilizing the interaction integral. The influence of minor cracks, holes and a combination of minor cracks and holes on the fracture properties of the main crack has been investigated. The impact of an elastic field and an electric displacement on intensity factors have been studied [49].

A wedge crack in a transverse isotropic PE material is explored under electromechanical loading. Note that a single anti-plane mechanical and in-plane electrical load is given to a spot on the wedge or crack surface. The Mellin transform is utilized to define the issue depending on the generalized displacement and stress vector. The resultant equation is solved utilizing the Wiener-Hopf method, the intensity factors and energy release rates are acquired in closed forms. Utilizing PZT-5H material specifications, the energy release rate and intensity factors for wedge and crack surface loadings are calculated numerically and assessed. Moreover, the closed-form solutions may be utilized as a Green's function for arbitrarily connected anti-plane mechanical and in-plane electrical loading scenarios [50]. The conclusions above are consistent with Guo J's research. J. Guo was interrogated. The electric field within the elliptical nano-hole was investigated, and the conformal mapping approach was used to calculate exact electroelastic fields around the elliptical nano-hole. Also, the sizedependent stress and electric displacement intensity factors at the

crack tip are calculated accurately for both electrically impermeable and permeable boundary conditions when the elliptical nano-hole shrinks to a nano-crack. Surface effects on electric displacement intensity factors and electrically impermeable and permeable crack stress, as well as electric field concentrations and stress in electrically impermeable and permeable holes, are quantitatively illustrated. The results reveal that an electrically permeable nano-hole or nano-crack has a various size dependency than an electrically impermeable nano-hole or nano-crack [51].

The imaging method is initially utilized to construct the essential function of Green's function, which fulfills the electric insulation and stress-free conditions on the horizontal boundaries in a right-angle space with a circular inclusion and bearing a harmonic out-plane line source force on the vertical boundary. The vertical border, on the other hand, splits the bimaterial medium into two portions. The first kind of Fredholm integral equations with unknown anti-plane forces are created utilizing the conjunction technique and crack-division technology. Besides, the integral equations are converted to algebraic equations with finite items utilizing effective truncation. Lastly, the DSIF at the crack tip and the dynamic stress concentration factor along the edge of the circular inclusion are determined. The dynamic stress concentration factor and

DSIF are described in relation to circular inclusion position, crack position, crack length, and incident wave frequency, among other aspects [52]. The conclusion is consistent with Yang G's prior findings, which indicate that the closed-form expression of electric displacement in cracks, stress, electrostatic fields, as well as field intensity components can be computed efficiently utilizing the expanded Stroh formalism. With rising remote loadings, the effects of Maxwell stress on the electric displacement intensity and stress components are studied utilizing numerical data. Besides that, we showed that an equivalent solution could be achieved from the scenario of a single crack when a reasonably lengthy duration (almost four times the crack length) is applied [53].

The electrical border condition is assumed to be semi-permeable in this case. Based on numerical results, the influence mechanism of electrostatic force and fracture speed is addressed [54]. In the course of his research, Viun O found that simple analytical formulae exist for the stresses at the interface as well as the intensity factors at the crack points. A finitesized PE bi-material plate having an interface crack whose length is much less compared to the plate diameter was studied utilizing the finite element method. The influence of polling direction on fracture parameters is examined. The

findings are displayed for a variety of polarization angles and material combinations. The analytical and numerical results are in good accord [55].

The displacement extrapolation technique is utilized to estimate the crack-tip field intensity factors of any arbitrarily kinked crack in linear PMs. By comparing BEM findings to current reference analytical data, the conclusions of the BEM are validated. Following that, the numerical differences between conventional field intensity factors and MERR of an infinitesimally kinked crack and hoop field intensity factors and hoop MERR of the primary crack prior to any kink are investigated. The propagation of cracks in an infinite linear PE material is eventually numerically simulated. To forecast the crack growth paths, the maximum hoop SIF and MERR crack criteria for the primary crack-tip before the upcoming propagation are used, as well as the optimum KI and MERR crack criteria for the kinked tip of the primary crack with an infinitesimal branch at an arbitrary kinking angle assessed using a trial crack e .

The results suggest that the present simplified approach may grant enough accuracy for numerical crack development modeling in linear PMs [56]. As per Rodriguez-Tembleque L., the research of the integrity of these materials in their many forms and small sizes is still a difficulty nowadays. In an attempt to get a deeper understanding of these systems,

this research provides a fracture surface contact formulation for evaluating the integrity of these innovative materials under highly realistic crack surface multifield operating circumstances. The BEM is utilized to calculate the elastic influence coefficients and contact operators over the augmented Lagrangian to enforce contact restrictions on the crack surface in the presence of electric fields. The abilities of this technique are demonstrated by solving a benchmark issue [57].

2.3. Ferromagnetic

Commonly, the MMM method is employed to quantitatively analyze crack and stress in ferromagnetic materials. Note that the inverse model includes the optimization parameters and objective function. The reconstruction technique is built utilizing the conjugate gradient inversion method as well as the exact line search algorithm. Moreover, the theoretical analysis employs an experimental signal with respect to a hole defect to demonstrate the utilization of the MMM technique in the quantitative assessment of defect size and position. The simulation findings are then utilized as observable signals in theoretical analyses of stress, fracture size, and location. The findings reveal that, among other aspects, the MMM method may be utilized to measure rectangular surface cracks, surface stress concentration zones, and convex-type defects. The signal

selection impact, stress level, lift-off value, sampling rate, as well as noise amplitude on the initial stress concentration's quantitative analysis is also comprehensively investigated [58]. The findings are in line with prior work by Qiu Q, who utilized ECPT to investigate the influence of tensile stress on crack depth quantification in ferromagnetic materials. Tests have been utilized to verify a theoretical study that included the ECPT theory, the stress equivalent field theory, as well as the μ -H σ curve. The results show that stress magnitude and direction have a considerable influence on thermal characteristics. Tensile stress may also raise the linear slope of the fracture depth quantitative curve. Moreover, POD curves reveal that tensile stress increases the ECPT capability to identify tiny cracks [59].

In this study, a novel DC electromagnetic NDT probe relying on the drag effect is developed. The sensing signal's sensitivity and intensity are determined by testing and then utilized to characterize cracks in high-speed moving ferromagnetic materials. After that, a multiconvolutional approach is utilized to investigate and calculate the detection signal's measurement ambiguity. The recommended probe may quantitatively characterize numerous cracks at 20 m/s with a 10% standard deviation and relative error when the crack depth is more than 1.0 mm. Subsequently, the better the experimental reproducibility, the greater the fracture. As a

consequence, the proposed probe should be capable of detecting numerous cracks in ferromagnetic materials moving at high speeds, for instance, high-speed railways, pipelines, and rotating bearings [60]. Also, Yuan F's prior study, which demonstrated the PEC technique's velocity effect by numerical simulation and testing, as well as the connections between PEC signal and speed, is compatible with the results. The results demonstrate that the velocity effect may alter the baseline value of the detection signal in the PEC detecting system. Additionally, when the crack appears in the high-level stage of the excitation signal, high-speed PEC can characterize the fracture location, width, and depth. Compared to static PEC testing, motion detection possesses a higher capacity to characterize crack depths. A novel high-speed inspection approach for fracture characterization in ferromagnetic material components, for instance, rotating rail tracks, pipelines, as well as metal components, are proposed depending on the results [61].

In ferromagnetic structures, if a deep flaw in the wall structure is present, only the shallower part of the defect within the skin-depth layer impacts the initial thermal response of IT. In contrast, the deeper area possesses minimal impact. This study offers a DCMIT approach for ferromagnetic materials that extends the visible depth range of standard IT.

Depending on permeability distortion in the skin-depth layer, DCMIT may be able to create a monotonic connection between the defect depth and the thermal feature. DCMIT can quantify the notch having a depth of up to 6.0 mm when the coil direction is parallel to the notch's length direction, whereas regular IT can barely manage this depth detection [62]. Furthermore, Yu C's earlier study, which strives to get a fundamental knowledge of the influence of multiple cracks on the fracture behavior of magnetoelastic materials, is compatible with the results. A soft ferromagnetic material degraded by an array of periodic fissures is explored theoretically under in-plane magnetic loading. Moreover, the conformal mapping technique and the analytic function boundary value theory are utilized to derive an analytical and rigorous solution for the stress and magnetic fields. Note that the closed-form equations for the field intensity components are provided. Utilizing numerical instances of magnetically permeable and impermeable cracks, the link between the mode-I stress intensity factor, the cracks' period ratio, the surrounding medium, as well as the applied magnetic loading is studied. The analytical solution found in this work may be utilized as a theoretical benchmark for the magnetoelastic fracture material with many flaws [7].

Firstly, the experimental results are utilized to verify the model's ECT simulation. The influence of crack size on induced voltage

is then researched. Four feature points of the imaginary and real sections of the induced voltage of the receiver coil are chosen to identify the crack size. Lastly, a Bayesian network is employed to predict the fracture size depending on the numerical simulation findings. According to the findings, the Bayesian network may precisely forecast the depth and width of tiny cracks [63]. The findings are consistent with those of prior Boughedda H research that employed the FEM. Apart from that, the FEM is employed to model the electromagnetic acoustic transducer (EMAT) response (output voltage) to the material under test in an attempt to establish a database for the inversion tool. Note that the second model employs the Partial Least Square Regression (PLSR) technique, which is a quick, simple, and precise inversion tool to determine the width and depth of surface cracks on the non-ferromagnetic materials. The PLSR approach for modeling the connection between a matrix of independent variables (predictors) (X) and a matrix of dependent variables (response)

(Y) (Y) is a dimensionality reduction method. By projecting original predictors into a new space with fewer dimensions, the PLSR aims to discover the Latent Variables (LV) with the highest prediction capability [64].

Since magnetic Barkhausen Noise (MBN)'s capacity to identify surface

fractures, fatigue loading of a martensitic stainless steel plate was managed, resulting in a portion via surface crack. The sample's surface was examined for BN emissions in incremental phases perpendicular and parallel to the crack. The strength of the MBN signal was measured and analyzed. While scanning the sample surface, localized peaks in the MBN measurements can identify the presence of faults. Furthermore, the observed MBN values can indicate the residual stress pattern both upstream and downstream of the crack tip. The findings suggest that doing a surface scan with MBN measurements can be a useful non-destructive approach for in situ NDT to identify and characterize surface cracks [15]. The findings are similar to Yang Z's previous research, which showed that increasing the heating duration to 6 seconds reduces the "proximity effect" of the coil and improves detection results. The tilted excitation approach worked effectively for cracks of varying depths. For the quantitative identification of fracture widths, the discontinuity point detection approach was presented. Aluminum specimens with penetrating cracks were analyzed utilizing the inclined excitation method, and the detection results were analyzed utilizing the wavelet singularity detection method. As a consequence, using inclined excitation in conjunction with wavelet singularity can significantly enhance thermographic images.

Under inclined excitation, crack temperature changes are comparable to those seen in numerical simulations, and the crack may be tracked more accurately and precisely [65]. For various loadings, the domain switching effect on the SIFs is examined. Domain switching enhances crack-tip intensity factors with respect to continuous stress loading, but domain switching lowers crack-tip intensity factors with respect to constant strain loading. Also, the findings show that the loading condition affects domain switching-induced anti-shielding or shielding of a fracture in ferromagnetic materials having an impermeable edge crack [66].

The MMM approach is used to quantitatively analyze crack and stress in ferromagnetic materials in this study. The objective function, as well as optimization parameters, are included in the inverse model. The conjugate gradient inversion method and the precise line search algorithm are utilized to create the reconstruction method. The feasibility of the MMM approach in the quantitative determination of defect size and position is proved in the theoretical analysis utilizing an experimental signal of a hole defect. Furthermore, theoretical assessments of stress and crack size and location are then carried out utilizing the simulation findings as observed signals. The findings suggest that the MMM approach may be utilized to quantify rectangular surface cracks, surface

stress concentration zones, and convex-type defects, among other things. The effects of noise amplitude, stress level, lift-off value, sampling rate, and signal selection on the early stress concentration's quantitative analysis are also thoroughly reviewed [58].

The equivalent source approach is utilized to investigate the multi-source effect of the magnetizing-based eddy current testing (MB-ECT) method in this study. The main magnetic leakage field, the secondary disturbed magnetic field, created the crack itself, as well as permeability distortion around the crack make up the disturbing magnetic field source. Moreover, FEA is performed to explore the impact of the magnetizing current and probe liftoff. As an outcome of the permeability distortion, the simulation result reveals a "concave" characteristic. The prominent signal components are analyzed in a series of tests under various conditions. When charting the signal amplitude as a function of the magnetizing current and probe lift-off in the MB-ECT technique, the magnetizing current selection correlates to a unique form. The multi-source effect in the MB-ECT sensors mechanism is revealed in this work, which also gives the core analysis or theory principles for accuracy crack assessment [20]. The wavelet energy's relative entropy of MMM signals is suggested to describe fatigue crack propagation predicated on the

attributes of time-frequency localization of information entropy and wavelet transform expressing the uncertainties of source information in MMM ferromagnetic materials' crack propagation. The crack propagation test examines the relative entropy of wavelet energy. The findings reveal that wavelet energy relative entropy is a sensitive indication of crack propagation. Furthermore, the length of crack propagation may be determined by the change region of wavelet energy's relative entropy. The crack depth is linearly proportional to the wavelet energy's relative entropy according to fracture analysis [22].

The stress field, paramagnetic field intensity, and ferromagnetic field intensity, obtained from Faraday's law of magnetic force line (uniform pure shear stress state), are employed to analyze this magneto-elastic stress problem accordingly. These three methods all provide a similar outcome: a uniform, pure shear stress condition. The kinked crack angles θ are reached for any direction δ of magnetic field intensity shortly after the crack initiation. The directions for $0^\circ \leq \delta \leq 360^\circ$ are taken into account. The accompanying three crack initiation criteria are factored:

- (i) With respect to the additional condition that the Mode I stress intensity factor is positive, the kinked crack forms in the direction that

takes the greatest value of the Mode I stress intensity factor shortly after the crack initiation;

(ii) The kinked crack begins in the direction where the Mode II stress intensity factor is equal to zero; (iii) With respect to the additional condition that the Mode II stress intensity factor is positive, the kinked crack forms in the direction that takes the highest value of the strain energy release rate.

The initiating angles are discovered to be in the range of $-150^\circ \leq \theta \leq 150^\circ$. These parameters, it is claimed, produce similar outcomes for kinked crack angles. For certain kinked crack angles and magnetic field intensity directions, the magnetic field intensity distributions and stress are explored. For various kinked crack angles, the stress intensity factors for certain magnetic field intensity directions are also explored vs. the crack length [22], [25].

3. Conclusion

This study review possibly provides three very popular themes in the field of cracking Crack Behaviour in Materials. To come to serve the base first, magnetoelastic plate in an electromagnetic field. Furthermore, the propagation of magnetoelastic plane waves having mechanical point loading causes a

moving Griffith crack in a self-reinforced strip of finite thickness and infinite extent with moving parallel punches of constant load acting on the strip's boundary on both sides. All of the cracking behavior depicted is the behavior of restricted cement materials in terms of cracking time and the use of least prone to crack concrete mixtures. Nevertheless, there has been little debate about the significance of this review analysis for settlement, which was to examine various current detection methods in an attempt to appeal to the diverse performance of existing procedures. The precision of the system's performance must be improved in an effort to design a new approach. Several of the review analyses potentially provide interventions from the significant research findings for the scholars reconciled with the classification method and the outstanding systems analysis, depending on the image's feature nucleus databases created in this work.

Author Contribution:

The following are the writers' contributions to the paper: flow and design of the study, collection of data: Amin, A.Z.M.; data interpretation: Amir, S., Amin; draft manuscript preparation: Kamali, M.Z.M. The outcomes were evaluated by all writers, and the finalized manuscript version was authorized.

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Conflicts of Interest:

The authors declare that they have no conflicts of interest to report regarding the present study.

Reference

- [1] L. Nazarenko, H. Stolarski, and H. Altenbach, "Effective properties of short-fiber composites with Gurtin-Murdoch model of interphase," *International Journal of Solids and Structures*, vol. 97, pp. 75–88, 2016, doi: 10.1016/j.ijsolstr.2016.07.041.
- [2] M. Keivani, A. Koochi, A. Kanani, M. R. Mardaneh, H. M. Sedighi, and M. Abadyan, "Using strain gradient elasticity in conjunction with Gurtin-Murdoch theory for modeling the coupled effects of surface and size phenomena on the instability of narrow nano-switch," *Proceedings of the Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science*, vol. 231, no. 17, pp. 3277–3288, 2017, doi: 10.1177/0954406216642475.
- [3] S. G. Mogilevskaya, A. Y. Zemlyanova, and V. Mantič, "The use of the GurtinMurdoch theory for modeling mechanical processes in composites with two-dimensional reinforcements," *Composites Science and Technology*, vol. 210, p. 108751, 2021, doi: 10.1016/j.compscitech.2021.108751.
- [4] P. Lu, R. Liu, H. Zhai, G. Wang, P. Yu, and C. Lu, "A modified beam model based on Gurtin–Murdoch surface elasticity theory," *Meccanica*, vol. 56, no. 5, pp. 1147–1164, 2021, doi: 10.1007/s11012-021-01312-8.
- [5] B. L. Wang and Y. W. Mai, "Applicability of the crack-face electromagnetic boundary conditions for fracture of magnetoelectroelastic materials," *International journal of solids and structures*, vol. 44, no. 2, pp. 387–398, 2007, doi: 10.1016/j.ijsolstr.2006.04.028.
- [6] Y. T. Zhou, S. J. Pang, and Y. H. Jang, "Magneto–electro interaction of two offset indenters in frictionless contact with magnetoelectroelastic materials," *Applied Mathematical Modelling*, vol. 52, pp. 197–214, 2017, doi: 10.1016/j.apm.2017.07.041.
- [7] D. Yang and G. Liu, "Anti-plane fracture problem of three nano-cracks emanating from a magnetoelectrically permeable regular triangle nano-hole in magnetoelectroelastic materials," *Modern Physics Letters B*, vol. 35, no. 7,

- p. 2150127, 2021, doi: 10.1142/S021798492150127X.
- [8] J. Li and X. B. Zhang, "Crack initiation prediction for v-notches under mixed-mode loading in brittle materials," *Journal of Mechanics of Materials and Structures*, vol. 1, no. 8, 2006, doi: 10.2140/jomms.2006.1.1385.
- [9] K. Jangid, "Electric and magnetic poling effects on two equal collinear semi-permeable cracks in magneto-electro-elastic materials," *ZAMM - Journal of Applied Mathematics and Mechanics / Zeitschrift für Angewandte Mathematik und Mechanik*, vol. 100, no. 12, p. e201900345, 2020, doi: 10.1002/zamm.201900345.
- [10] T. H. Lengyel and P. Schiavone, "Displacement field in an elastic solid with mode-III crack and first-order surface effects," *Journal of Mechanics of Materials and Structures*, vol. 7, no. 8–9, 2012, doi: 10.2140/jomms.2012.7.783.
- [11] M. Lowengrub and N. I. M. Noordhoff, "Some Basic Problems of the Mathematical Theory of Elasticity.," *The American Mathematical Monthly*, vol. 74, no. 6, 1967, doi: 10.2307/2314307.
- [12] D. S. Kryzhevich, A. V Korchuganov, and K. P. Zolnikov, "Effect of excess atomic volume on crack evolution in a deformed iron single crystal," *Materials*, vol. 14, no. 20, p. 6124, 2021, doi: 10.3390/ma14206124.
- [13] L. Daniel and M. Domenjoud, "Anhysteretic magneto-elastic behaviour of Terfenol-D: Experiments, multiscale modelling and analytical formulas," *Materials*, vol. 14, no. 18, p. 5165, 2021, doi: 10.3390/ma14185165.
- [14] L. Ren, K. Yu, and Y. Tan, "Applications and advances of magnetoelastic sensors in biomedical engineering: A review," *Materials*, vol. 12, no. 7, p. 1135, 2019, doi: 10.3390/ma12071135.
- [15] J. Wu, J. Zhu, and G. Y. Tian, "Depth quantification of surface-breaking cracks in ferromagnetic materials using DC-biased magnetization based induction thermography," *Mechanical Systems and Signal Processing*, vol. 141, p. 106719, 2020, doi: 10.1016/j.ymssp.2020.106719.
- [16] C. Yu, C. F. Gao, and Z. Chen, "Periodically spaced collinear cracks in a soft ferromagnetic material under a uniform magnetic field," *Acta Mechanica*, vol. 231, no. 5, pp. 1919–1931, 2020, doi: 10.1007/s00707-020-02629-3.
- [17] G. E. Tupholme, "Stack of non-uniformly loaded shear cracks in magnetoelectroelastic materials," *Mechanics of Advanced Materials and*

- Structures*, pp. 1–9, 2020, doi: 10.1080/15376494.2020.1716119.
- [18] Y. Stoyanov, P. Dineva, and T. Rangelov, “2D problems in magneto-electro-elastic materials with a nano-crack,” *AIP Conference Proceedings*, vol. 3283, no. 2, p. 070001, 2019, doi: 10.1063/1.5133537.
- [19] T. H. Wu and X. Y. Li, “Elliptical crack problem in magneto-electro-thermo-elasticity of transversely isotropic materials: 3D analytical and numerical solutions,” *International Journal of Engineering Science*, vol. 144, p. 103136, 2019, doi: 10.1016/j.ijengsci.2019.103136.
- [20] Y. Z. Liu, J. H. Guo, and X. Y. Zhang, “Surface effect on a nano-elliptical hole or nanocrack in magnetoelectroelastic materials under antiplane shear,” *ZAMM - Journal of Applied Mathematics and Mechanics / Zeitschrift für Angewandte Mathematik und Mechanik*, vol. 99, no. 7, p. e201900043, 2019, doi: 10.1002/zamm.201900043.
- [21] Y. Stoyanov, “2D crack problems in functionally graded magneto-electro-elastic materials,” in *Engineering Design Applications*, A. Öchsner and H. Altenbach, Eds. Cham, Switzerland: Springer Nature, 2019, pp. 255–265. doi: 10.1007/978-3-319-79005-3_18.
- [22] E. Jeoffroy, F. Bouville, M. Bueno, A. R. Studart, and M. N. Partl, “Iron-based particles for the magnetically-triggered crack healing of bituminous materials,” *Construction and Building Materials*, vol. 164, pp. 775–782, 2018, doi: 10.1016/j.conbuildmat.2017.12.223.
- [23] Z. Deng, Y. Kang, J. Zhang, and K. Song, “Multi-source effect in magnetizing-based eddy current testing sensor for surface crack in ferromagnetic materials,” *Sensors and Actuators A: Physical*, vol. 271, pp. 24–36, 2018, doi: 10.1016/j.sna.2018.01.009.
- [24] H. T. Liu, Y. H. Qie, and Z. G. Zhou, “Investigation of non-local theory solution to a three-dimensional rectangular permeable crack in magneto-electro-elastic materials,” *International Journal of Mechanical Sciences*, vol. 134, pp. 460–478, 2017, doi: 10.1016/j.ijmecsci.2017.10.039.
- [25] X. Nan, C. Zhigang, J. Aiwei, M. Yanfan, N. Yang, and T. Ming, “The relative entropy of wavelet energy of Metal Magnetic Memory signal used in feature analysis of crack propagation in ferromagnetic materials,” in *2017 Prognostics and System Health Management Conference (PHM-Harbin)*, 2017, pp. 1–4. doi: 10.1109/PHM.2017.8079219.
- [26] N. Hasebe and N. Omatsu, “Analysis of a kinked crack in soft ferromagnetic and paramagnetic elastic materials subjected to uniform magnetic field intensity,”

- Engineering Fracture Mechanics*, vol. 184, pp. 141–153, 2017, doi: 10.1016/j.engfracmech.2017.08.032.
- [27] X. Y. Li, G. Z. Kang, and Y. H. Li, “Failure of materials! smart materials and structures thermo-magneto-electro-elastic fundamental field in an infinite space weakened by a pennyshaped crack subjected to a pair of point temperature loads,” in *ICF 2017 - 14th International Conference on Fracture (ICF 2017)*, 2017, pp. 742–743.
- [28] H. Qi, F. Chu, J. Guo, and R. Sun, “Dynamic analysis for a vertical interface crack and the nearby circular cavity located at the piezoelectric bi-material half-space under SH-waves,” *Acta Mechanica*, vol. 232, no. 3, pp. 1113–1129, 2021, doi: 10.1007/s00707-020-02812-6.
- [29] R. Kumar, H. Pathak, A. Singh, and M. Tiwari, “Modeling of crack repair using piezoelectric material: XFEM approach,” *Engineering Computations: International Journal for Computer-Aided Engineering*, vol. 38, pp. 586–617, 2020, doi: 10.1108/EC-01-2020-0001.
- [30] X. Wang and P. Schiavone, “Electroelastic field for a blunt crack in an anisotropic piezoelectric material,” *Continuum Mechanics and Thermodynamics*, vol. 33, no. 6, pp. 2509–2514, 2021, doi: 10.1007/s00161-021-01035-x.
- [31] N. An and T. S. Song, “Dynamic fracture behavior for functionally graded piezoelectric bi-materials with interfacial cracks near a circular hole,” *Waves in Random and Complex Media*, pp. 1–19, 2021, doi: 10.1080/17455030.2021.1936284.
- [32] N. An, T. Song, and G. Hou, “Dynamic performance for piezoelectric bi-materials with an interfacial crack near an eccentric elliptical hole under anti-plane shearing,” *Mathematics and Mechanics of Solids*, vol. 27, no. 1, pp. 93–107, 2022, doi: 10.1177/10812865211014924.
- [33] H. T. Liu, P. H. Wang, and Y. H. Qie, “Non-local stress and electric displacement solution of a 3D semi-permeable rectangular crack in infinite orthotropic piezoelectric materials,” *ZAMM - Journal of Applied Mathematics and Mechanics / Zeitschrift für Angewandte Mathematik und Mechanik*, p. e202000309, 2021, doi: 10.1002/zamm.202000309.
- [34] S. Zhu and H. Liu, “Finite element analysis of the three-dimensional crack and defects in piezoelectric materials under the electro-mechanical coupling field,” *Journal of Intelligent Material Systems and Structures*, vol. 32, no. 15, pp. 1662–1677, 2021, doi: 10.1177/1045389X20983884.
- [35] G. Pamnani, S. Bhattacharya, and S. Sanyal, “Numerical simulation of tri-

- layer interface cracks in piezoelectric materials using extended finite element method,” *Iranian Journal of Science and Technology, Transactions of Mechanical Engineering*, vol. 44, no. 4, pp. 905–917, 2020, doi: 10.1007/s40997-019-00307-x.
- [36] C. Srinivasu and S. K. Yadav, “A XFEM approach for the three-dimensional cracks in piezoelectric material using interaction integral,” *Engineering Fracture Mechanics*, vol. 239, p. 107322, 2020, doi: 10.1016/j.engfracmech.2020.107322.
- [37] R. Kumar, A. Singh, and M. Tiwari, “Investigation of crack repair using piezoelectric material under thermo-mechanical loading,” *Journal of Intelligent Material Systems and Structures*, vol. 31, no. 19, pp. 2243–2260, 2020, doi: 10.1177/1045389X20943946.
- [38] A. Sheveleva, V. Loboda, and Y. Lapusta, “A conductive crack and a remote electrode at the interface between two piezoelectric materials,” *Applied Mathematical Modelling*, vol. 87, pp. 287–299, 2020, doi: 10.1016/j.apm.2020.06.003.
- [39] H. T. Liu, “Dynamic intensity factors for multiple permeable cracks in piezoelectric materials,” *ZAMM - Journal of Applied Mathematics and Mechanics / Zeitschrift für Angewandte Mathematik und Mechanik*, vol. 100, no. 9, p. e201900344, 2020, doi: 10.1002/zamm.201900344.
- [40] N. An, T. S. Song, and G. Hou, “Interfacial cracks near an eccentric circular hole in piezoelectric bi-materials subjected to dynamic incident anti-plane shearing,” *AIP Advances*, vol. 10, no. 5, p. 055009, 2020, doi: 10.1063/1.5110575.
- [41] E. M. Craciun, A. Rabaea, and S. Das., “Cracks Interaction in a pre-stressed and prepolarized piezoelectric material,” *Journal of Mechanics*, vol. 36, no. 2, pp. 177–182, 2020, doi: 10.1017/jmech.2019.57.
- [42] N. An, T. S. Song, M. Zhao, Y. Liu, and G. Hou, “Dynamic performance analysis of interfacial cracks near an eccentric elliptical hole in piezoelectric bi-materials under incident SH-waves,” in *Pressure Vessels and Piping Conference*, 2020, pp. 1–9. doi: 10.1115/PVP2020-21416.
- [43] N. An, T. S. Song, G. Hou, B. Yang, and H. Pan, “Dynamic anti-plane analysis for interfacial cracks emanating from an eccentric circular cavity in piezoelectric bi-materials,” *Waves in Random and Complex Media*, vol. 31, no. 6, pp. 2197–2213, 2021, doi: 10.1080/17455030.2020.1736687.
- [44] P. Pei, G. Yang, Y. Shi, and C. Gao, “Periodic interfacial cracks in dissimilar

- piezoelectric materials under the influence of Maxwell stress,” *Meccanica*, vol. 55, no. 1, pp. 113–124, 2020, doi: 10.1007/s11012-019-01110-3.
- [45] L. Rodríguez-Tembleque, F. García-Sánchez, and A. Sáez, “Crack-face frictional contact modelling in cracked piezoelectric materials,” *Computational Mechanics*, vol. 64, no. 6, pp. 1655–1667, 2019, doi: 10.1007/s00466-019-01743-x.
- [46] Z. H. U. Shuai and H. T. Liu, “Fracture analysis of multiple cracks in functionally graded piezoelectric materials based on layering method,” in *2019 14th Symposium on Piezoelectricity, Acoustic Waves and Device Applications (SPAWDA)*, 2019, pp. 1–6. doi: 10.1109/SPAWDA48812.2019.9019244.
- [47] H. Liu and S. Zhu, “Dynamic analysis of two collinear permeable Mode-I cracks in piezoelectric materials based on non-local piezoelectricity theory,” *Multidiscipline Modeling in Materials and Structures*, vol. 15, no. 6, pp. 1274–1293, 2019, doi: 10.1108/MMMS-122018-0215.
- [48] O. Onoprienko, V. Loboda, A. Sheveleva, and Y. Lapusta, “Bond zone model for a conductive crack at the interface of piezoelectric materials under anti-plane mechanical and inplane electric loadings,” *ZAMM - Journal of Applied Mathematics and Mechanics / Zeitschrift für Angewandte Mathematik und Mechanik*, vol. 99, no. 9, p. e201800230, 2019, doi: 10.1002/zamm.201800230.
- [49] H. T. Liu, J. G. Wu, and T. J. Li, “Dynamic analytical solution of a limited-permeable mode-I crack in piezoelectric materials based on the non-local theory,” *Wave Motion*, vol. 90, pp. 82–98, 2019, doi: 10.1016/j.wavemoti.2019.05.003.
- [50] R. Mishra, R. G. Burela, and H. Pathak, “Crack interaction study in piezoelectric materials under thermo-electro-mechanical loading environment,” *International Journal of Mechanics and Materials in Design*, vol. 15, no. 2, pp. 379–412, 2019, doi: 10.1007/s10999018-9410-0.
- [51] J. Cheng, B. Sun, M. Wang, and Z. Li, “Analysis of III crack in a finite plate of functionally graded piezoelectric/piezomagnetic materials using boundary collocation method,” *Archive of Applied Mechanics*, vol. 89, no. 2, pp. 231–243, 2019, doi: 10.1007/s00419-018-1462-y.
- [52] G. Pamnani, S. Bhattacharya, and S. Sanyal, “Analysis of interface crack in piezoelectric materials using extended finite element method,” *Mechanics of*

- Advanced Materials and Structures*, vol. 26, no. 17, pp. 1447–1457, 2019, doi: 10.1080/15376494.2018.1432817.
- [53] S. R. Choi and I. Chung, “Asymmetric impermeable wedge crack in a piezoelectric material under anti-plane deformation,” *Journal of Mechanical Science and Technology*, vol. 32, no. 10, pp. 4767–4773, 2018, doi: 10.1007/s12206-018-0924-z.
- [54] J. Guo and X. Li, “Surface effects on an electrically permeable elliptical nano-hole or nano-crack in piezoelectric materials under anti-plane shear,” *Acta Mechanica*, vol. 299, no. 10, pp. 4251–4266, 2018, doi: 10.1007/s00707-018-2232-1.
- [55] H. Qi and X. M. Zhang, “Scattering of SH-wave by a circular inclusion near the interfacial cracks in the piezoelectric bi-material half-space,” *Journal of Mechanics*, vol. 34, no. 3, pp. 337–347, 2018, doi: 10.1017/jmech.2017.7.
- [56] G. Yang and C. F. Gao, “The influence of maxwell stress on the periodical cracks in piezoelectric material,” in *Proceeding of the 2017 Symposium on Piezoelectricity, Acoustic Waves, and Device Applications (SPAWDA)*, 2017, pp. 303–307. doi: 10.1109/SPAWDA.2017.8340345.
- [57] L. Q. Qi, Y. Shi, and C. F. Gao, “The influence of electrostatic force on the moving interfacial crack between dissimilar piezoelectric materials,” in *Proceeding of the 2017 Symposium on Piezoelectricity, Acoustic Waves, and Device Applications (SPAWDA)*, 2017, pp. 319–324. doi: 10.1109/SPAWDA.2017.8340348.
- [58] O. Viun, A. Komarov, Y. Lapusta, and V. Loboda, “A polling direction influence on fracture parameters of a limited permeable interface crack in a piezoelectric bi-material,” *Engineering Fracture Mechanics*, vol. 191, pp. 143–152, 2018, doi: 10.1016/j.engfracmech.2018.01.024.
- [59] J. Lei and C. Zhang, “A simplified evaluation of the mechanical energy release rate of kinked cracks in piezoelectric materials using the boundary element method,” *Engineering Fracture Mechanics*, vol. 188, pp. 36–57, 2018, doi: 10.1016/j.engfracmech.2017.07.008.
- [60] L. Rodríguez-Tembleque, F. García-Sánchez, and A. Sáez, “Crack surface frictional contact modelling in piezoelectric materials,” *Key Engineering Materials*, vol. 774, pp. 607–612, 2018, doi: 10.4028/www.scientific.net/KEM.774.6
- [61] P. Shi, K. Jin, P. Zhang, S. Xie, Z. Chen, and X. Zheng, “Quantitative inversion of stress and crack in ferromagnetic materials based on metal magnetic memory method,” *IEEE Transactions on*

- Magnetics*, vol. 54, no. 10, pp. 1–11, 2018, doi: 10.1109/TMAG.2018.2856894.
- [62] Q. Qiu, J. Wu, X. Chen, H. Xia, M. Zhang, and J. Zhu, “Tensile stress effect on crack depth quantification in ferromagnetic materials using ECPT,” *Measurement*, vol. 182, p. 109740, 2021, doi: 10.1016/j.measurement.2021.109740.
- [63] F. Yuan, Y. Yu, W. Wang, and G. Tian, “A novel probe of DC electromagnetic NDT based on drag effect: design and application in crack characterization of high-speed moving ferromagnetic material,” *IEEE Transactions on Instrumentation and Measurement*, vol. 70, pp. 1–10, 2021, doi: 10.1109/TIM.2021.3069036.
- [64] F. Yuan, Y. Yu, B. Liu, and G. Tian, “Investigation on velocity effect in pulsed eddy current technique for detection cracks in ferromagnetic material,” *IEEE Transactions on Magnetics*, vol. 56, no. 9, pp. 1–8, 2020, doi: 10.1109/TMAG.2020.3012341.
- [65] J. Song and Y. Zhao, “Quantitative evaluation of surface crack in ferromagnetic materials based on Bayesian network in eddy current testing,” *International Journal of Applied Electromagnetics and Mechanics*, vol. 64, pp. 1–4, 2020, doi: 10.3233/JAE-209423.
- [66] H. Boughedda, T. Hacib, Y. Le Bihan, and H. Acikgoz, “Cracks characterization of non-ferromagnetic material using EMAT probe and PLSR technique,” *Progress In Electromagnetics Research C*, vol. 103, pp. 199–209, 2020, doi: 10.2528/PIERC20013103.
- [67] Y.-W. Chen and G.-C. Tsai, “The Crack of Turbine Blade Effect on the Dynamic Behavior of Turbine,” *Journal of Applied Mathematics and Physics*, vol. 02, no. 06, 2014, doi: 10.4236/jamp.2014.26045.
- [68] G. Zhao, “Numerical Comparison Research on the Solution of Stress Intensity Factors of Multiple Crack Problems,” *Advances in Pure Mathematics*, vol. 10, no. 12, 2020, doi: 10.4236/apm.2020.1012044.
- [69] T. M. Dinka and R. J. Lascano, “Review Paper: Challenges and Limitations in Studying the Shrink-Swell and Crack Dynamics of Vertisol Soils,” *Open Journal of Soil Science*, vol. 02, no. 02, 2012, doi: 10.4236/ojss.2012.22012.